

# Two-phase anaerobic co-digestion of organic waste and activated sludge:

bench study & implementation potential in energy and material (VFA) recovery

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#### **BACKGROUND**

The two-phase anaerobic digestion approach physically divides into 2 steps the biogas producing process:

- 1. dark fermentation  $\cdot$   $\cdot$  Bio-hydrogen (H<sub>2</sub>)
- 2. methanogenesis •••> Bio-methane (CH<sub>4</sub>)

Bio-hydrogen + Bio-methane → **BioHythane** 

50-55% CH<sub>4</sub>, 5-10% H<sub>2</sub> & 35-40% CO<sub>2</sub>

BioHythane allows a better combustion with reduced greenhouse gasses emissions compared with fossil fuels.

- Process stability = pH 5.5
- Controlled by codigestion of biowaste & waste activated sludge (WAS)
- Dark fermentation produces
- a low chain carbon rich stream to enhance denitrification kinetics in WWTP

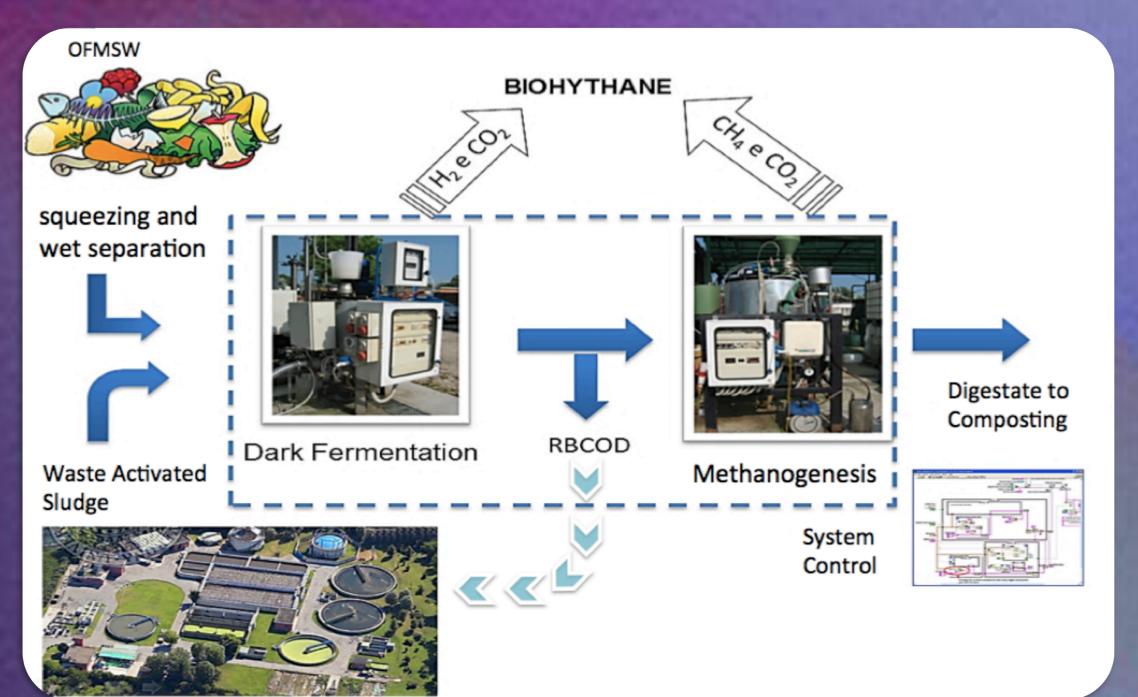


Figure 1. Scheme of process

Integrate waste and wastewater cycles:

THE GOAL

Experimental results are used to evaluate the benefits coming from the implementation of this technology in a full scale WWTP, using as model a real plant located in north Italy (70.000 PE basin).

### MATERIAL AND METHODS

Two laboratory-scale CSTR. Experiment length 70 d.

The substrate employed in this study was a mix of BIOWASTE & WAS. The volume ratio BIOWASTE:WAS was 1:5 v/v. Reactor effluents were monitored daily & analyses performed according to APHA (1995).

Table 1. Operational conditions

		Dark fermentation	Methanogenesis
HRT	d	3	16
OLR	kgTVS/m <sup>3</sup> d	16	3
Temperature	°C	55	55
Reactor volume	L	3.5	18.5

#### RESULTS AND DISCUSSION

- Process performances and yields are summarized in Table 2.
- > rbCOD RECOVERY FOR BIOLOGICAL NUTRIENT REMOVAL

Application scenario in Treviso WWTP by **Upscaling** of the studied process

the RBCOD needed to the N removal is

given by the cycle integration

the complete mass balance of the whole approach in Figure 2.

Table 2. Effluents characteristics and specific yields

	Parameters	Units	Dark fermentation	Methanogenesis
	TS	g/kg	48±5	25±4
	TVS	g/kg	37±4	16±2
	COD	g/kg TS	40±3	19±2
	TKN	g/kg TS	34±1	35±1
	Ptot	g/kg TS	11±0	19±1
	рН		5.09±0.08	7.97±0.26
	Partial Alkalinity (pH = 5.7)	mgCaCO <sub>3</sub> /I	NP	3328±165
	Total Alkalinity (pH = 4.3)	mgCaCO <sub>3</sub> /I	1210±180	4409±16
	$NH_4^+ - N$	$mgN-NH_4^+/I$	268±48	949±48
	Tot VFA	gCOD/l	15.8±1.4	0.5±0.5
	Yields			
	SHP	I H <sub>2</sub> /kg TVS	29±5	np
	SMP	I CH <sub>4</sub> /kg TVS	np	287±36

The hydrogen production is 156.2 m<sup>3</sup>H<sub>2</sub>/d

treating whole available sludge and 13.1 t/d of biowaste

First phase effluent with VFA 15.8 gCOD/I:

> 62 m<sup>3</sup>/d to BNR COD required to denitrify the water entering in the plant is 1038 kg/d

> 864 m³/d, is channeled to the methanogenic reactor

Methane production of  $1032.6 \, \text{m}^3/\text{d}$ 

The system is able to support a complete denitrification in WWTP using less than the 15.2 % of the total carbon which is produced by the first phase reactor. Total production of 1921 m<sup>3</sup>/d of Biohythane with an average % composition of 54/8/38 as CH<sub>4</sub>/H<sub>2</sub>/ CO<sub>2</sub> respectively.

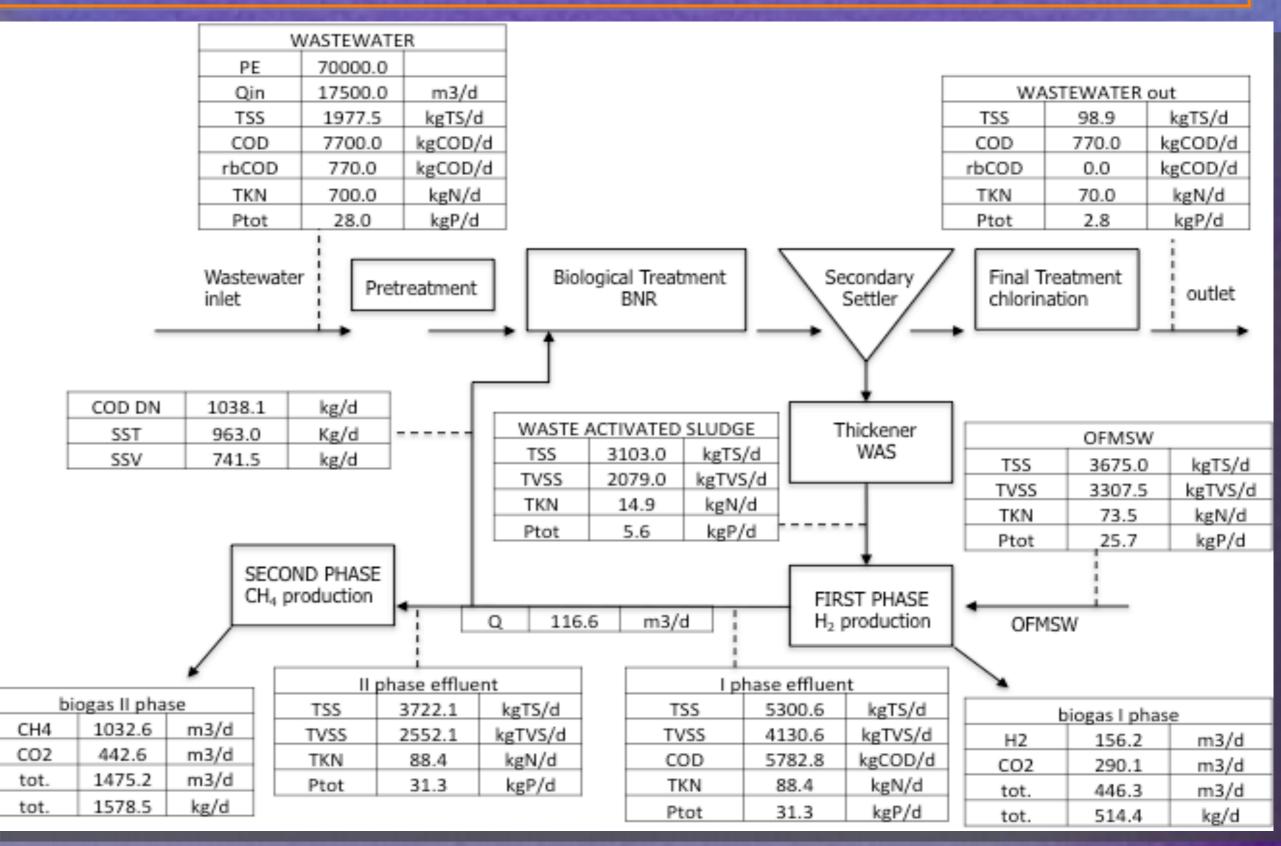


Figure 2. Complete mass balance of upscaling

#### CONCLUSIONS

The integrated approach has considerable advantages in the field of the 'smart' opportunities for the urban services management.

On a 70.000 PE basis

- $H_2$  production of 156.2 m<sup>3</sup>/d &  $CH_4$  of 1032.6 m<sup>3</sup>/d;
- Reduction of CO<sub>2</sub> emissions
- Total wastewater denitrification is reached through yield of 426 gVFA/kgTVS<sub>fed</sub>(first-phase), which leads to a specific denitrification rate of 5.5 kgN/kgMLVSS h.
- External chemicals for denitrification are not utilized

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## **REFERENCES**

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